## UNIVERSAL FRICTION LAW FOR TURBULENT BOUNDARY LAYERS WITH WALL SUCTION

Igor Vigdorovich

Institute of Mechanics, Moscow State University, Moscow, Russia

<u>Abstract</u> A universal friction law for turbulent boundary layers on a flat plate with suction is established. Experimental skin-friction distributions obtained for various suction factors and Reynolds numbers are described in similarity variables by a single universal curve. The law is valid for the entire range of suction velocities from zero one till the limiting values corresponding to asymptotic-suction boundary layers. The analysis is not based on any particular turbulence model.

## **PROBLEM FORMULATION**

We consider an incompressible turbulent boundary-layer flow over a smooth flat plate with a constant free-stream velocity  $u_e$  and a constant wall suction velocity  $v_w$  parallel to the normal vector. The origin of the Cartesian coordinate system is situated at the leading edge of the plate.

**Closure condition.** In the flow under consideration, any mean quantity is a function of Cartesian coordinates x and y and only three governing parameters: the kinematic viscosity  $\nu$ , the free-stream velocity  $u_e$ , and the suction velocity  $v_w$ . This means that the gradient of the stream-wise mean-velocity component, the turbulent shearing stress, and the boundary-layer thickness can be represented in terms of universal functions:

$$\frac{\partial u}{\partial y} = F_1(x, y, \nu, u_e, v_w), \quad \langle u'v' \rangle = F_2(x, y, \nu, u_e, v_w), \quad \Delta = F_3(x, \nu, u_e, v_w). \tag{1}$$

We solve the first and third equations in (1) for x and  $u_e$  and substitute them into the second one to obtain the relation  $\langle u'v' \rangle = F_4(\Delta, y, \nu, \partial u/\partial y, v_w)$ , which after applying dimensional considerations yields

$$\langle u'v' \rangle = -\left(y\frac{\partial u}{\partial y}\right)^2 S(\operatorname{Re},\,\beta,\,\eta), \quad \operatorname{Re} = \frac{y^2}{\nu}\frac{\partial u}{\partial y}, \quad \beta = \frac{v_w}{y\partial u/\partial y}, \quad \eta = \frac{y}{\Delta}.$$
 (2)

Here, S is some universal function of three variables. The local Reynolds number Re is defined here as the ratio of characteristic turbulent and molecular viscosity values, the parameter  $\beta$  characterizes suction affect on shearing stress. **Change of variables.** The mean-flow stream function  $\psi(x, y)$  satisfies the boundary-layer equation for zero-pressuregradient flow:

$$\psi_y \psi_{xy} - \psi_x \psi_{yy} = (\nu \psi_{yy} - \langle u'v' \rangle)_y; \quad x > 0, \quad y = 0: \quad \psi_y = 0, \quad \psi_x = -v_w; \quad y \to \infty: \quad \psi_y \to u_e.$$
(3)

We perform in this equation the following change of variables [1]:  $\psi = u_e \Delta \Psi(\xi, \eta), \xi = \ln \text{Re}_\Delta$ , where  $\text{Re}_\Delta = u_e \Delta/\nu$ , using the logarithm of the Reynolds number  $\text{Re}_\Delta$  based on the boundary-layer thickness and the normalized distance from the wall  $\eta$  as independent variables. With the closure condition (2), Eq. (3) becomes

$$\Lambda[\Psi_{\eta}\Psi_{\xi\eta} - (\Psi + \Psi_{\xi})\Psi_{\eta\eta}] = \left[ (\eta\Psi_{\eta\eta})^{2} S(\operatorname{Re}, \beta, \eta) + e^{-\xi}\Psi_{\eta\eta} \right]_{\eta}, \quad \operatorname{Re} = e^{\xi}\eta^{2}\Psi_{\eta\eta}, \quad \beta = B \left(\eta\Psi_{\eta\eta}\right)^{-1};$$
  
$$\xi > -\infty, \quad \eta = 0: \quad \Psi = 0, \quad \Psi_{\eta} = 0, \quad \Lambda(\Psi + \Psi_{\xi}) = -B; \quad \eta \to \infty: \quad \Psi_{\eta} \to 1.$$
(4)

Here,  $B = v_w/u_e$  is the suction factor. Besides the normalized stream function  $\Psi$ , Eq. (4) contains the second unknown function  $\Lambda(\xi) = d\Delta/dx$ . We will seek an asymptotic solution to the problem (4) as  $\xi \to \infty$ , i. e. for high values of the logarithm of the Reynolds number based on the boundary-layer thickness. We introduce a small parameter  $\varepsilon$  and a new independent variable  $\zeta = \varepsilon \xi$ ,  $1/\zeta = O(1)$ . We specify the suction factor as  $B = \varepsilon^2 b$ , b = O(1).

## SOME RESULTS

Wall region. In the outer part of the wall region, in the logarithmic sublayer, the velocity profile obeys the similarity law

$$\frac{2}{v_{+}}\left(\sqrt{1+v_{+}u_{+}}-1\right) = \frac{1}{\varkappa}[\ln y_{+} + C(v_{+})] + O\left(y_{+}^{-\alpha}\right), \quad y_{+} \to \infty, \quad \alpha > 0.$$
(5)

Here, the accustomed wall variables are used, in particular  $v_+ = B/\sqrt{\frac{1}{2}c_f}$ , where  $c_f$  is the skin-friction coefficient, and  $\varkappa = \sqrt{S(\infty, 0, 0)}$ . For  $v_+ = 0$ , in the limiting case of an impermeable wall, Eq. (5) reduces to the normal log law, hence  $\varkappa$  is the von Kármán constant equal to 0.41 and  $C(v_+) = C_0 + O(v_+)$ ,  $v_+ \to 0$ , where  $C_0 = 2.05$ . Since  $B = O(\varepsilon^2)$  and





**Figure 1.** Velocity profile near the suction wall in turbulent Poiseuille flow with a constant wall transpiration [2] plotted in similarity variables (5). The straight line has the equation  $\frac{1}{0.41}(\ln y_+ + 2.05)$ .

**Figure 2.** Experimental data on skin friction [3, 4] plotted in terms of scaling variables (8);  $\bigcirc$ , [3],  $\square$ , [4] (indirect measurements),  $\blacksquare$ , [4] (measured with floating elements).

 $\sqrt{\frac{1}{2}c_f} = O(\varepsilon)$ , the parameter  $v_+ = O(\varepsilon)$ , i. e. is always a small quantity. The similarity law (5) is perfectly supported by the recently obtained DNS data [2]. Figure 1 shows the calculated velocity profile for the pressure-driven turbulent plane channel flow (Poiseuille flow) with a constant transverse mass flux. The velocity profile near the suction wall corresponds to  $v_+ = -0.0305$ . Plotted in variables (5), it has a distinct logarithmic potion, which is very close to that for the velocity profile near an impermeable wall.

**Outer region of the boundary layer.** In the outer region of the boundary layer we seek the solution in the form of following asymptotic expansions:

$$\Lambda(\xi) = -\varepsilon^2 b\,\lambda(s) + O(\varepsilon^3), \quad \Psi(\xi,\,\eta) = \Psi_w(\xi) + \eta - \varepsilon^2 b\,g(s,\,\eta) + O(\varepsilon^3), \quad s = \frac{1}{\varepsilon} \left(\zeta - \frac{2\varkappa}{\sqrt{-b}}\right) - k\ln(-b\varepsilon^2), \quad (6)$$

where k is a certain coefficient. After substituting Eqs. (6) in Eq. (4) we obtain for the functions g and  $\lambda$  a partial differential equation

$$\left[ \left( \eta g_{\eta\eta} \right)^2 S(\infty, \beta, \eta) \right]_{\eta} + (1 + \eta \lambda) g_{\eta\eta} = \lambda g_{s\eta}, \quad \beta = -(\eta g_{\eta\eta})^{-1}; \quad g(s, 0) = g_{\eta}(s, \infty) = g_{\eta\eta}(s, \infty) = 0.$$
(7)

**Friction law.** The universal friction law is obtained as a result of asymptotic matching of the solutions for the outer and wall regions making use of the inner-solution asymptotics (5) and the corresponding wall asymptotics of the solution to the boundary-value problem (7). The law has the following formulation:

$$Z_{\left\{\begin{smallmatrix}\delta^*\\x\end{smallmatrix}\right\}} \equiv (-B)^{\mp 1} \sqrt{\frac{c_f}{2}} \exp\left(\frac{2\varkappa\sqrt{\frac{1}{2}c_f}}{B}\right) \operatorname{Re}_{\left\{\begin{smallmatrix}\delta^*\\x\end{smallmatrix}\right\}} = \Phi_{\left\{\begin{smallmatrix}1\\2\end{smallmatrix}\right\}}\left(\frac{\sqrt{\frac{1}{2}c_f + B}}{-B}\right) + O(\sqrt{c_f}).$$

$$\tag{8}$$

Here,  $\operatorname{Re}_x$  and  $\operatorname{Re}_{\delta^*}$  are the Reynolds numbers based on the distance from the leading edge of the plate and the boundarylayer displacement thickness, respectively,  $\Phi_1$  and  $\Phi_2$  are some universal functions. It is valid for the entire range of suction velocities from zero one till the limiting values corresponding to asymptotic-suction boundary layers and, as figure 2 shows, is in perfect agreement with experimental data [3, 4]. The data cover a vide range of Reynolds numbers  $4 \leq \operatorname{Re}_x \cdot 10^{-5} \leq 20$  and suction factors  $1.2 \leq -B \cdot 10^3 \leq 2.4$  for [3] and  $3.8 \leq \operatorname{Re}_x \cdot 10^{-5} \leq 35$  and  $1 \leq -B \cdot 10^3 \leq 3.6$ for [4]. Plotted in terms of similarity variables (7), all experimental points follow a single curve in figure 2.

## References

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